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“A Novel approach to reduce Torpedo ladle relining turnaround time”

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Introduction

Torpedo availability is critical for hot metal transportation from Blast furnaces to LD Shops, considering the limited fleet, which is required for daily production at Tata Steel, Jamshedpur plant. Low torpedo availability can lead to low HM buffer & interruption in HM supply to LD Shops. Relining is a major activity (longest downtime) of torpedo maintenance so reduction in torpedo relining turnaround time will increase the availability of torpedo.



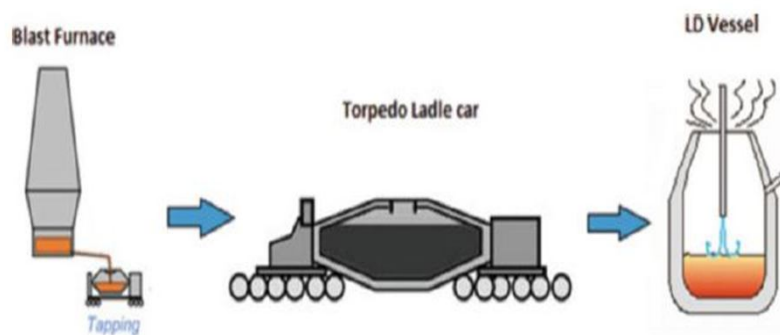
Current challenges:

- High Hot metal production
- Carbon foot print reduction- Environment friendly
- Cost pressure
- Easy , flexible and safe workbility



Current Practices and methods(1/2)

- At Tata Steel - Jamshedpur works; a fleet of 48 refractory-lined, steel torpedo ladles are used to transport the hot metal from six Blast Furnaces to three LD shops.
- There are two types of torpedo ladle, consisting of 320Mt capacity and 200Mt capacity. .
- At present 21nos of 200t and 27nos 320 t TLCs are in fleet to transport 32000 tons of hot metal per day



| Parameters | 320t TLC | 200t TLC |
|-----------------------------------------|----------------------|--------------------|
| Vessel capacity with new lining | 320t | 200t |
| Hot metal temperature (deg C) | 1550 | 1550 |
| Weight of TLC (without refractory) | 180 ton | 113 ton |
| Weight of TLC (with refractory) | 300 t (approx) | 218t |
| Inside volume of vessel with new lining | 51.23 m ³ | 39.5m ³ |
| Available free board | 2.27 m ³ | 1.8m ³ |
| Overall height of car above rail top | 4350 mm | 4110 mm |
| Overall width of car | 3500 mm | 3428mm |
| Max. permissible shell temperature | 300 deg C | 300 deg C |
| Overall refractory thickness | 400 mm | 400 mm |

Technical specification of Torpedo ladle cars

Current Practices and methods(2/2)

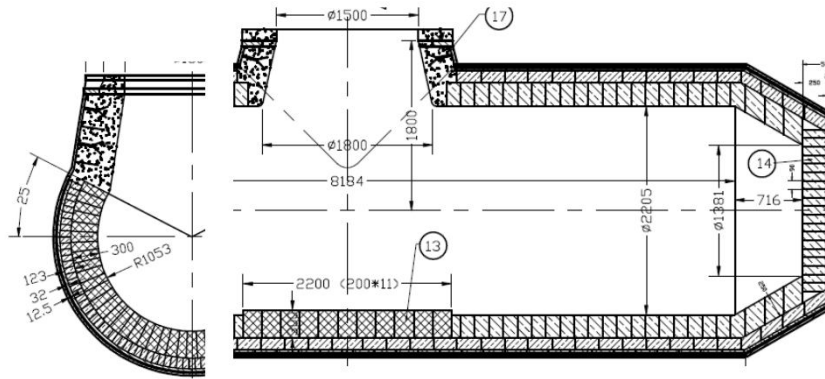


Fig. 2: Lining configuration of 200t torpedo ladle

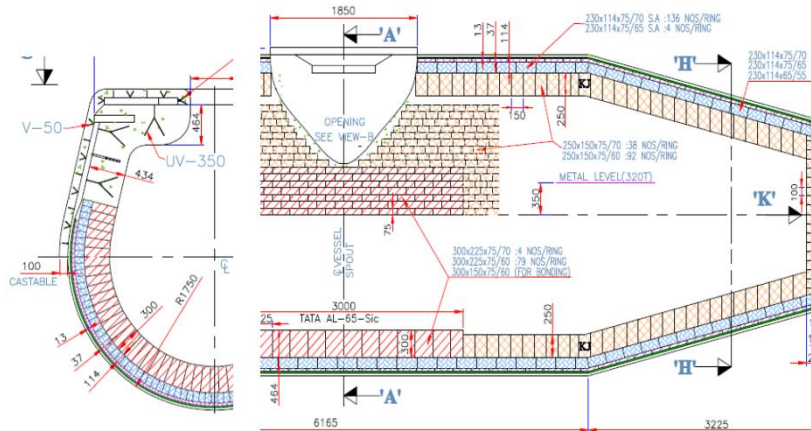
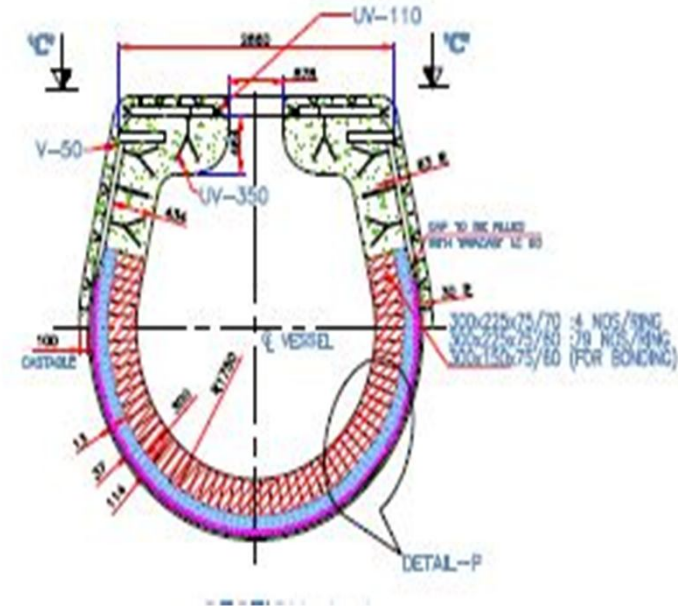


Fig. 3: Lining configuration of 320t torpedo ladle



Lining configuration of spout portion of 320t torpedo ladle

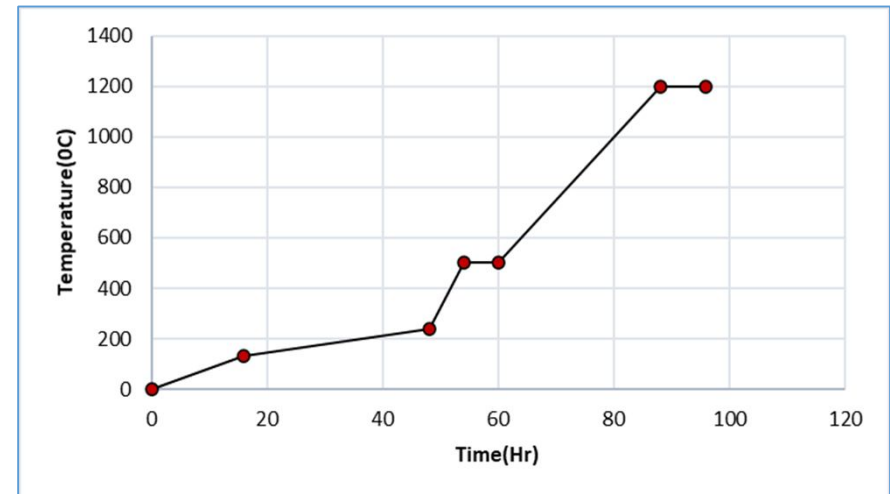
Activities performed for Torpedo repairing

| Sl no | Activities details | Time(Hours) |
|-------|-------------------------------------------------------------|-------------|
| 1 | Cooling | 16 |
| 2 | Dismantling | 64 |
| 3 | Mechanical+ Elecrical+other repair | 48 |
| 4 | Refractory relining | 204 |
| 5 | End wall lining, shield plate casting and end cover closing | 24 |
| 6 | Heating | 96 |
| Total | | 452 |

Relining is a major activity (longest downtime) of torpedo maintenance. reduction in torpedo relining turnaround time will increase the availability of torpedo. Current turnaround time for a newly lined torpedo 452 Hours, which includes 96 hours. of preheating schedule.

Issues with current Spout Low cement castable:

- Higher drying time
- Low self life (9 months)
- formation of low melting compounds, namely, anorthite ($\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot 2\text{SiO}_2$) and gehlenite ($2\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot \text{SiO}_2$)
- High energy consumption**



Existing Heating schedule of new relined torpedo

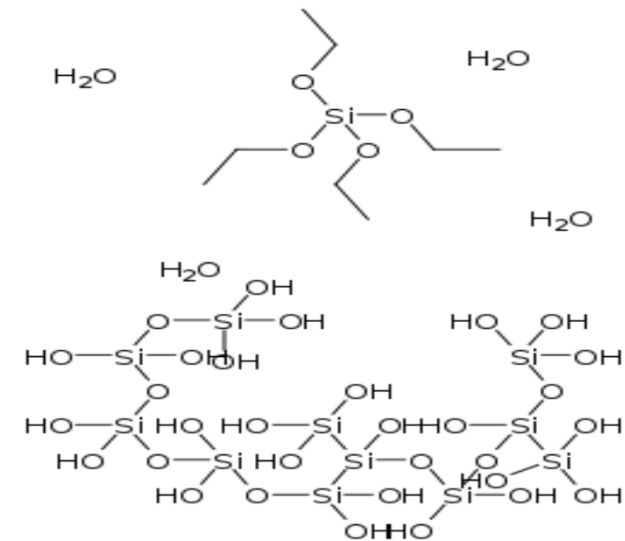
Introduction to No cement based castable (NCC)

Benefits of NCC over LCC :

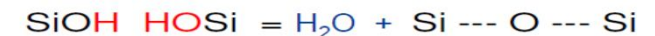
- ❑ Reduced drying time and drying defects due to the absence of free water for mixing and permeable structure.
- ❑ Inherent formation of mullite in alumina compositions improves corrosion resistance and hot strength properties.
- ❑ Better high-temperature properties due to absence low melting compounds in CaO–Al₂O₃–Fe₂O₃ and CaO–Al₂O₃–SiO₂ systems.
- ❑ Better high-temperature properties result in longer campaign life and reduced downtime of operation.

Future of castable : NCC

Drying mechanism of Silica SOL



Silica Sol Gelation Process



Their main characteristics are shown in **Table** and compared with the existing torpedo spout castable.

| Sample type | Existing castable | Trial sample-1 (T-1) | Trial sample-2 (T-2) |
|-------------------------------------------------|----------------------------|---------------------------------|-------------------------------------------------------------|
| Base material/ Bonding type | High Alumina Cement bonded | Mullite based Silica Sol bonded | Al ₂ O ₃ -SiC based Silica Sol bonded |
| CHEMICAL ANALYSIS(%) | | | |
| ELEMENT DESCRIPTION | ANALYSIS | | |
| CaO | 2.42 | 0.6 | 0.5 |
| SiO ₂ | 9.9 | 31.28 | 27.22 |
| Fe ₂ O ₃ | 1.07 | 1.04 | 1.18 |
| Al ₂ O ₃ | 83.03 | 63.36 | 56.47 |
| TiO ₂ | 2.26 | 1 | 1.09 |
| SiC | - | - | 11.78 |
| OTHER PROPERTIES | | | |
| WATER (%) | 6 | - | - |
| Silica SOL (%) | - | 8.3 | 8.9 |
| @110 ^o C BULK DENSITY(g/cc) | 2.8 | 2.42 | 2.42 |
| @110 ^o C POROSITY (%) | 14.7 | 14.22 | 15.2 |
| @110 ^o C CCS kg/cm ² | 640 | 600 | 580 |
| @1000 ^o C BULK DENSITY(g/cc) | 2.77 | 2.43 | 2.42 |
| @1000 ^o C CCS (kg/cm ²) | 780 | 825 | 927 |
| @1000 ^o C PLC(%) | -0.24 | -0.06 | -0.04 |
| @1400 ^o C BULK DENSITY(g/cc) | 2.73 | 2.44 | 2.44 |
| @1400 ^o C CCS (kg/cm ²) | 867 | 945 | 962 |
| @1400 ^o C PLC(%) | 0.59 | -0.19 | -0.1 |
| Corrosion Index | ++ | ++ | + |
| RTE @1000 ^o C(%) | 0.75 | 0.5 | 0.62 |
| Thermal conductivity' @800 ^o C(W/mK) | 1.78 | 1.47 | 1.46 |

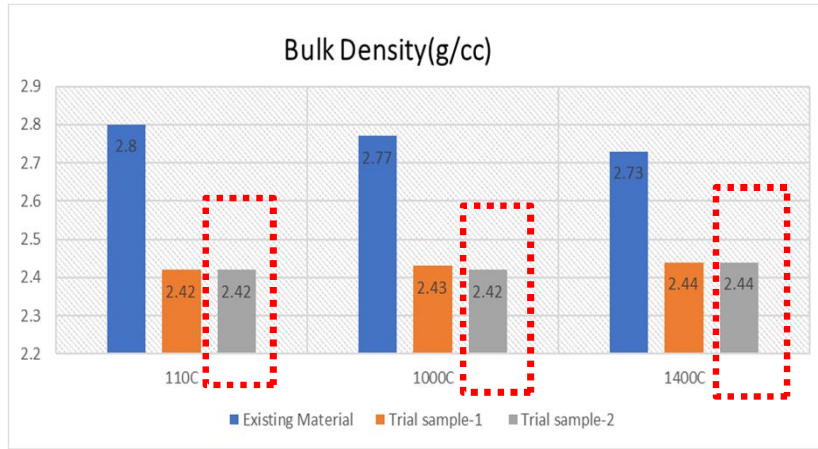
Chemical composition

- Very low lime percentage found in case of both trial Sol bonded castables due to usage of silica sol as binder in place of high alumina cement.
- Trial -2 contains Silicon carbide, whereas no SiC is present in trial-1 and existing castable.
- Less alumina percentage found in trial NC castables.

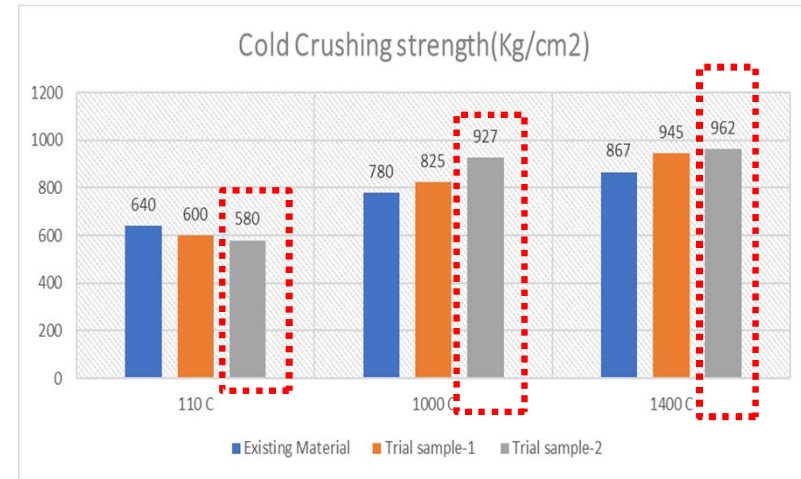
- ✓ Existing castable : LCC HAC bonded
- ✓ Trial Sample -1 : Mullite based Silica Sol bonded castable
- ✓ Trial sample-2 : Alumina- SiC based Silica Sol bonded castable

Results and discussions

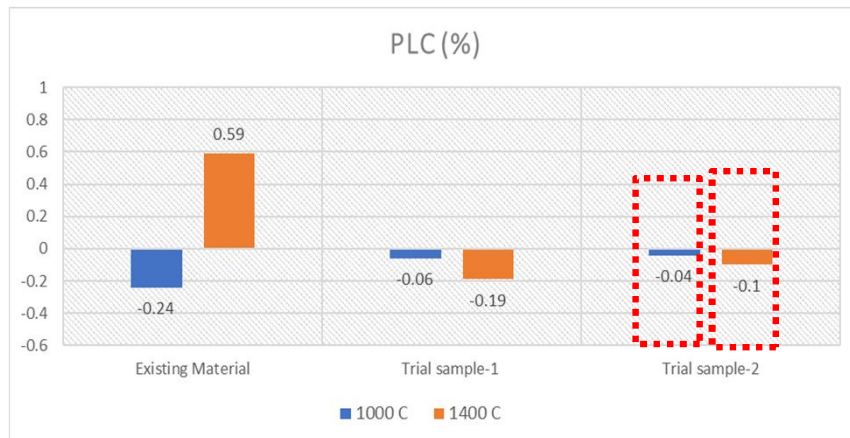
Physical and other properties



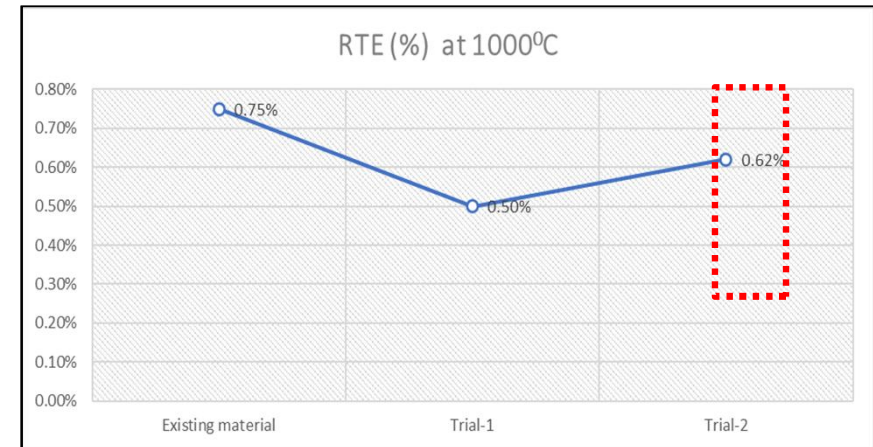
Bulk density values at three different temperature



Strength values at three different temperature

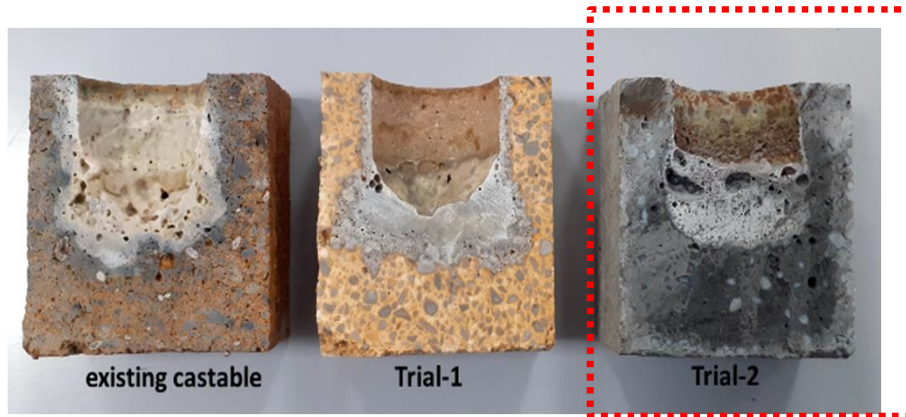


PLC values at three different temperature



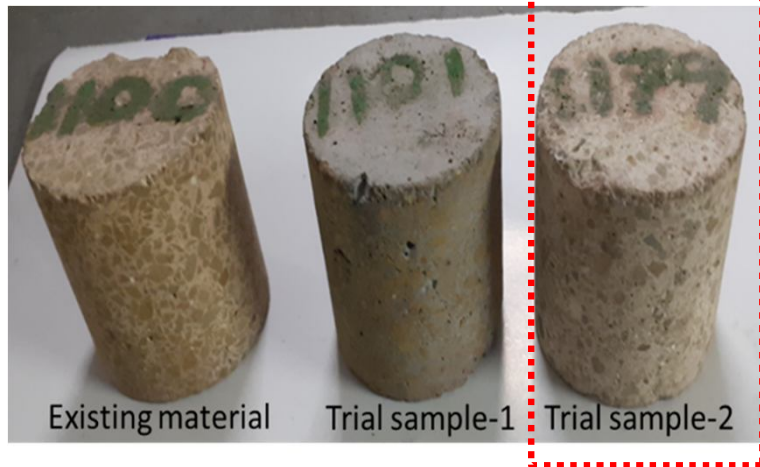
Thermal expansion % at 1000 deg C

Thermomechanical properties

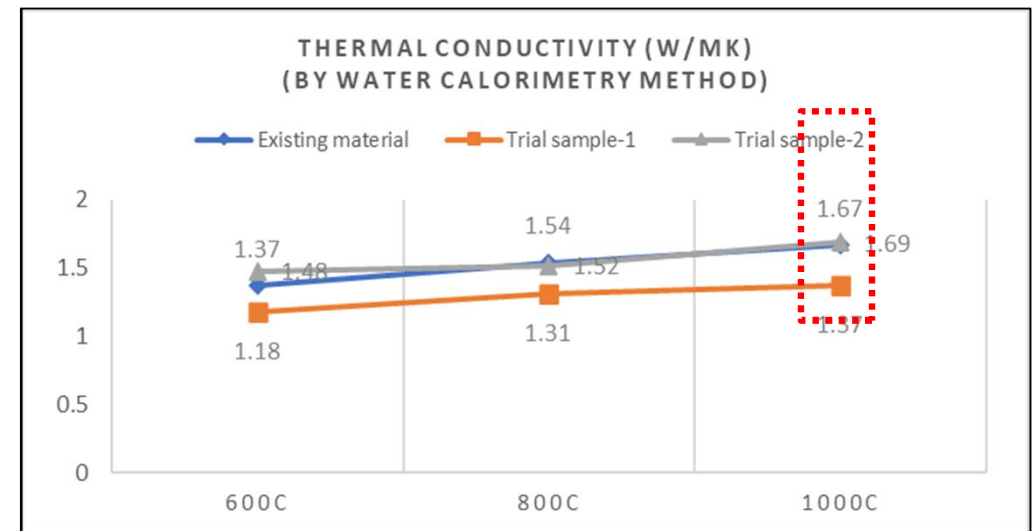


Corrosion test with BF slag after firing at 1500 C/ 3hrs

| Corrosion index | | |
|-------------------|--------|----|
| Existing material | 72.20% | ++ |
| Trial -1 | 80% | ++ |
| Trial -2 | 26.50% | + |



Results of thermal spalling after 50 cycle



Results of thermal conductivity test

Application of Trial castable

SiC based sol bonded castable shown better refractory properties (Trial Sample-2) as compared to the existing cement bonded castable and the other mullite based sol bonded material.

- Better high temp. properties
- High corrosion resistance against BF slag
- Comparable thermal conductivity values

Based on all the analysis; **SiC based sol bonded castable** finalized to take trial for Torpedo Mouth application and to validate the actual performance at the site.

TRIAL DETAILS

| | |
|----------------------|------------------------|
| Date of Trial | 15-05-2022 |
| Torpedo No | 41 |
| Material used | Sol bonded castable |
| Application area | Torpedo mouth/ Spout |
| Qty of material used | ~ 8Mt |
| Binder used | Silica Sol |
| Binder addition (%) | 9.5 |
| Template removed | after 24hrs of casting |
| Heating period | 62 hrs |



Condition of torpedo spout after preheating



Spout templates

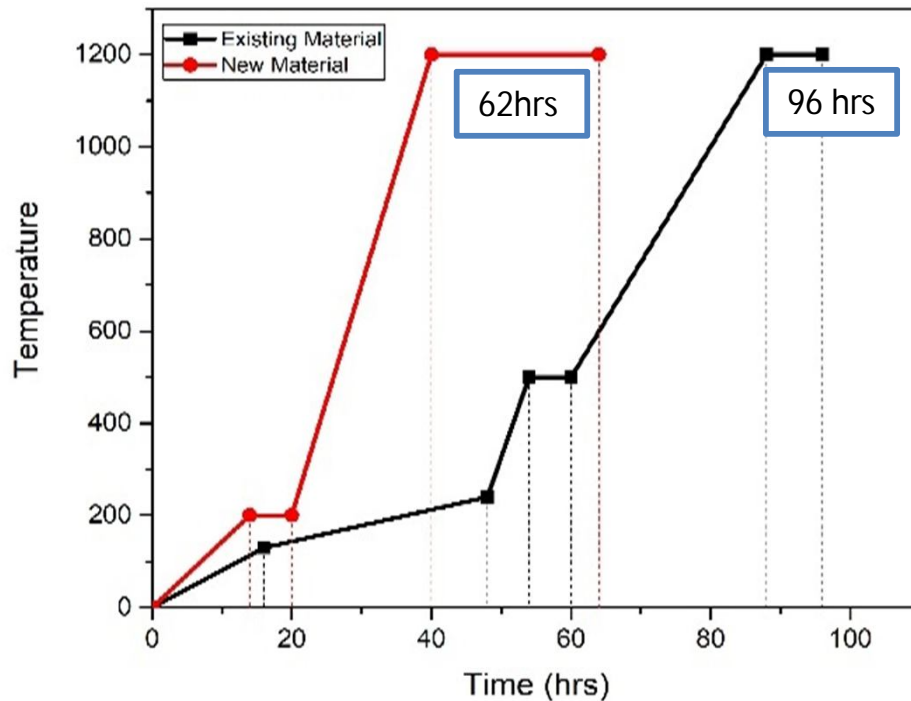


During casting



after casting

Comparative heating schedule existing Vs Trial



Findings :

- ✓ Reduced drying time by 34hrs
- ✓ Very long shelf life (18 months)
- ✓ Reduction of CO gas consumption by 30%
- ✓ Lower consumption of repair material (like gunning consumption) due better high temp. properties
- ✓ Reduced Shell temperature within the safety norms (<300 Deg C) due to lower thermal conductivity values
- ✓ Enhanced corrosion resistance due to presence of SiC
- ✓ longer campaign life and reduced downtime of operation.

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THANK YOU