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Paper name: Interaction between refractory and liquid steel regarding steel cleanliness



PRESENT AFFILIATION

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AREAS OF INTEREST

Steel Making and Product Development

B.Sc (Engg)
M.Tech Met Engg
PGPM
Ph.D (Pursuing)

NIT-Jamshedpur
IIT (BHU), Varanasi
IMT, CDL Ghaziabad
AcSIR-NML Jamshedpur

Experience

- 12 Years exp. in Project & Operation in Blast Furnace/ Steel making at Neelachal Ispat Nigam Ltd, Kalinganagar, Odisha
- 8 years exp. in R&D in steel & product area at Bokaro Steel Plant

Projects:

- 110 t BOF & LHF- Erection and Hot Commissioning
- RFID Technology for ladle management in steel melting shop
- Ni-Coating of Cu-mould for increasing mould life at CCS,BSL
- Anti-Flaking Treatment of defense grade steel at BSL
- Product Development: Thinner Gauge LPG HS345, Ferritic Nano-precipitate formable grade steel HS600, API X60/X65/X70, SAILFORMING, HSFQ, SBQ, EDD, Cold rolled annealed HSLA steel
- High strength high coating galvanized steel

Publication

- 40 publications and presentations in national & international journals
- 3 nos. of patents & 1 no of Copy-right



Interaction between Refractory and Liquid Steel Regarding Steel Cleanliness



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Steel cleanliness is the one unifying theme in all steel plants as problems in steel cleanliness can lead to internal rejects or customer dissatisfaction with steel products. Thus all steel plants are continually attempting to improve their practices to produce more consistent products.

Three main keys for quality steel production

- **Chemistry,**
- **Inclusion control and**
- **Rolling parameter**

Reason of Focus on inclusion

The first is their influence on the properties and the quality of steel products. This is a significant aspect from the point of view of steel product users, who have to take into account the presence of inclusions in evaluating the material behaviour in working condition.

Despite of small content of non-metallic inclusions in steel they exert significant effect on the steel properties such as:

- Tensile strength
- Deformability (ductility)
- Toughness
- Fatigue strength
- Electrical properties

❖ Thermal Expansion:

- ❖ MnS, CaS etc. have a thermal expansion greater than steel matrix.
 - void or parting of the matrix can occur. The void act as crack
- ❖ Al_2O_3 , SiO_2 , MgO, $\text{CaO} \cdot \text{Al}_2\text{O}_3$ etc have a thermal expansion smaller than steel matrix
 - internal stresses developed

- Mechanism of inclusion formation:

Indigenous inclusions are formed in liquid, solidified or solid steel as a result of chemical reactions (deoxidation, desulfurization) between the elements dissolved in steel.

Exogenous inclusions are derived from external sources such as furnace refractories, ladle lining, mold materials etc.

- In industrial practice, the inclusions of MgO are found in liquid steel, and those inclusions may come from erosion of refractory lining. MgO-based inclusions are formed in steel as a result of the erosion of vessel lining refractory or as a chemical reaction product.
- Erosion of refractories, is a very common source of large exogenous inclusions which are typically solid and related to the materials of the ladle and tundish themselves. They are generally large and irregular-shaped.

- Exogenous inclusions have the following common characteristics:
 - Large size: Inclusions from refractory erosion are generally larger than those from slag entrainment.
- Compound composition/ multiphase, cause by the following phenomena:
- Due to the reaction between molten steel and SiO_2 , FeO , and MnO in the slag and lining refractory, the generated Al_2O_3 inclusions may stay on their surface;

Exogenous inclusions

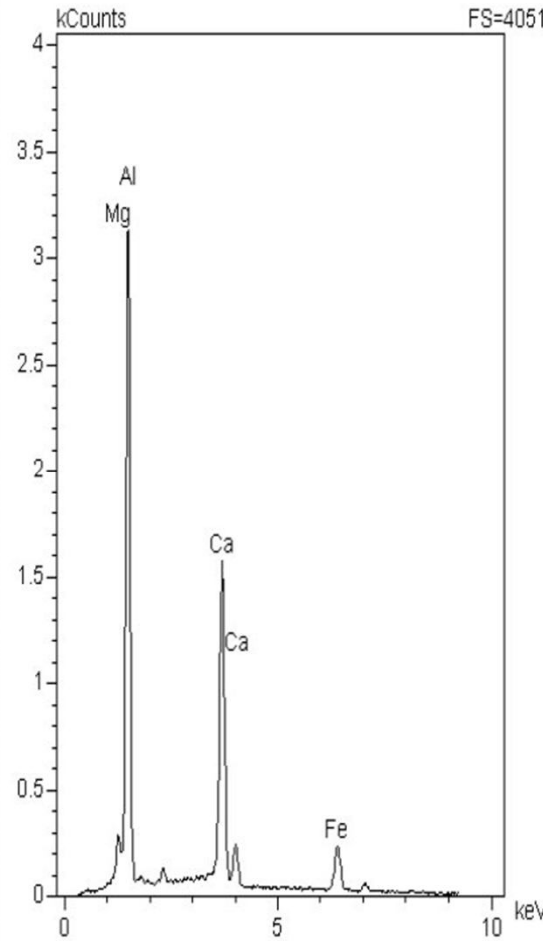
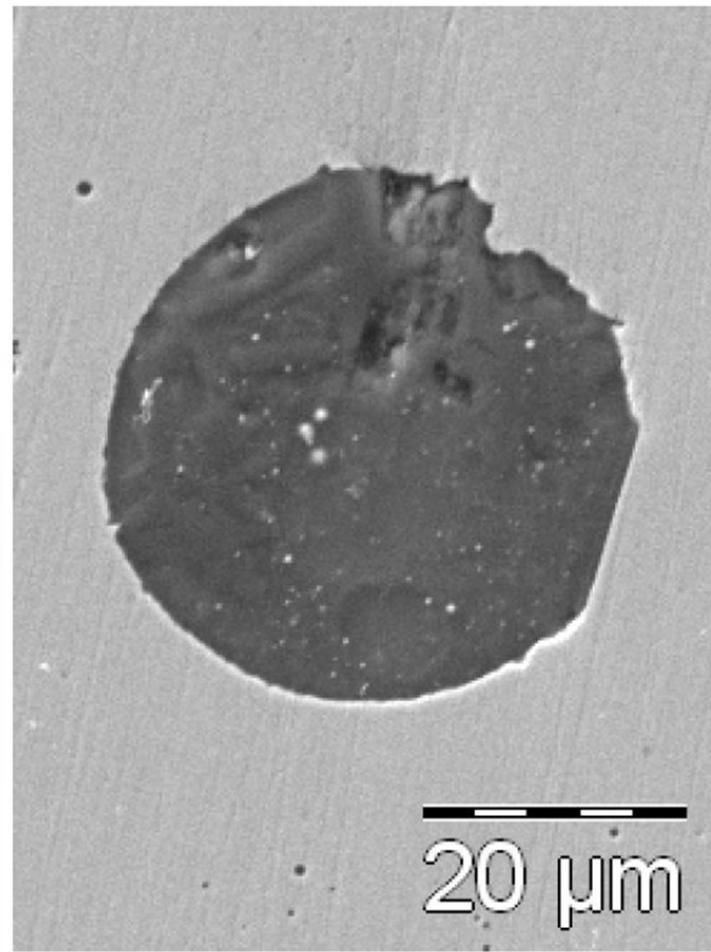


- As exogenous inclusions move, due to their large size, they may entrap deoxidation inclusions such as Al_2O_3 on their surface
- Exogenous inclusions act as heterogeneous nucleus sites for precipitation of new inclusions during their motion in molten steel
- Slag or reoxidation inclusions may react with the lining refractories or dislodge further material into steel.
- Irregular shape, if not spherical from slag entrainment or deoxidation product silica. The spherical exogenous inclusions are normally large ($>50\mu m$) and mostly multiphase, but the spherical deoxidation inclusions are normally small and single phase.

- MgO-containing solid or liquid inclusions, such as magnesia (MgO), spinel (MgO $_$ Al₂O₃), forsterite (2MgO $_$ SiO₂), and (3CaO $_$ Al₂O₃)-MgO clusters are formed during steelmaking processes, deoxidation treatment or by reactions with MgO rich alkaline slags.
- The steel/slag reaction time influences strongly the type, composition, and shape of inclusions. With increase of reaction time, solid blocky/rectangular-shaped MgO $_$ Al₂O₃ and MgO-based inclusions were transferred into CaO–MgO–Al₂O₃ system inclusions with a low melting temperature <1500 $_$ C.

- They change their shape to semi-spherical or spherical. The solid magnesia and spinel inclusions “would be inevitably and gradually transferred into complex liquid inclusions even dissolved [Ca] is as low as 0.0002%”. Inclusions with an MgO–Al₂O₃ or Mg-based core surrounded by a CaO–Al₂O₃ surface layer with a lower melting temperature were detected.
- In addition, depending on the quality of the used magnesite in the refractory and the slag composition, the proportion of SiO₂ and CaO leads to low melting compounds at processing conditions. Thus, the corrosion of the refractory material is promoted.

Oxide Inclusion

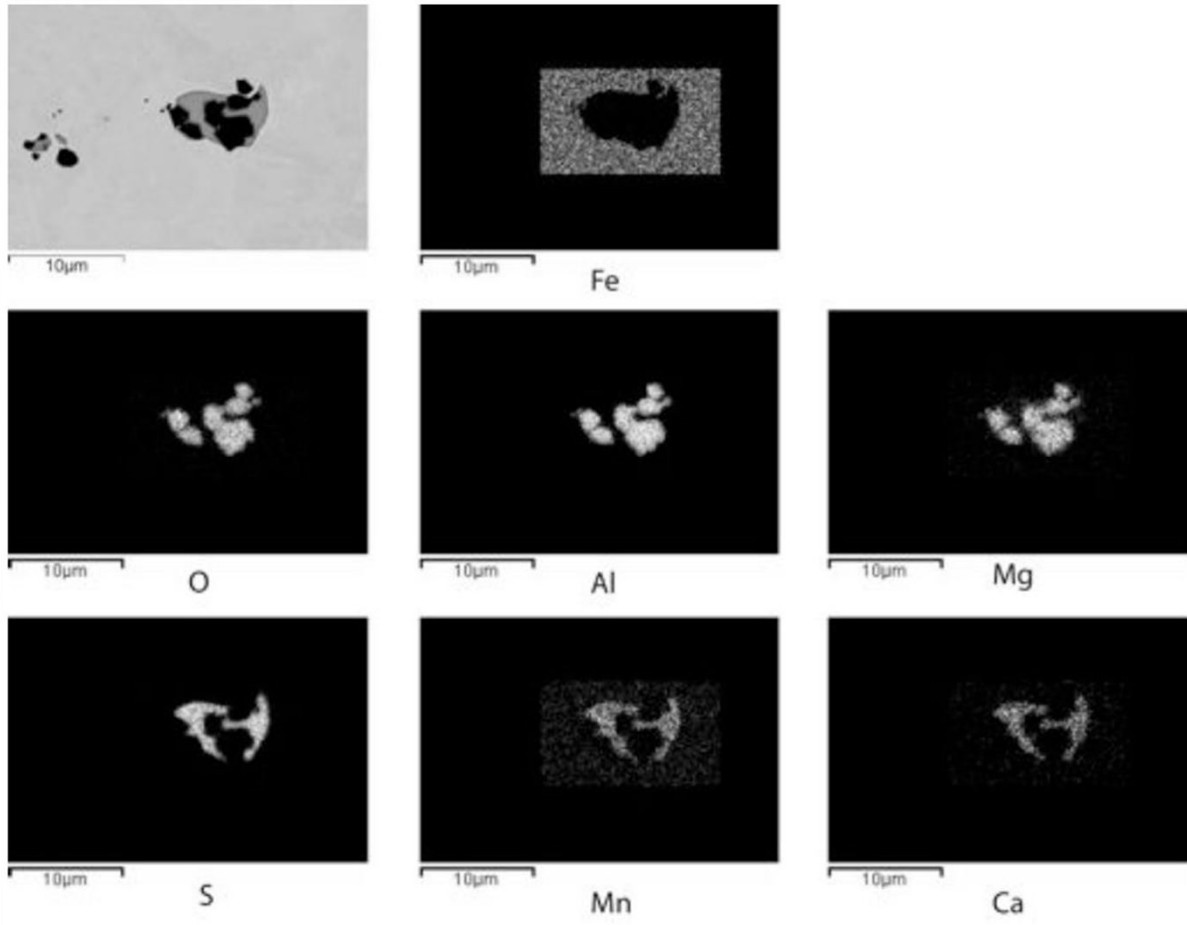


Steel composition:

0.10% C,
0.64% Mn,
0.01% P,
0.005% S,
0.13% Si,

Oxide inclusions

complex oxy-sulfide inclusion in steel



Inclusion name: Complex inclusions

Inclusion type: Micro

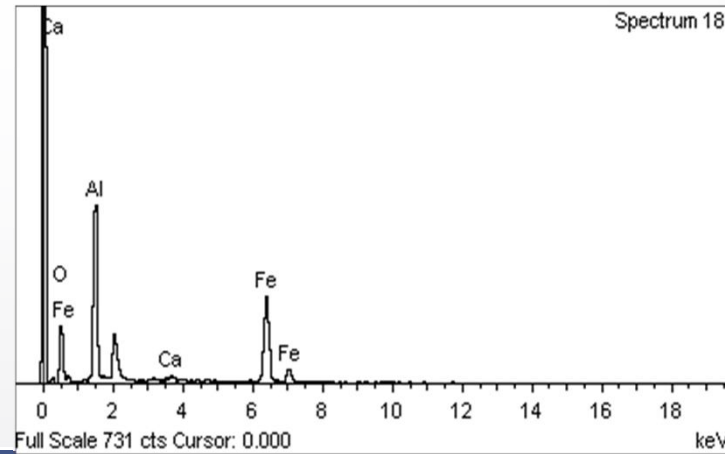
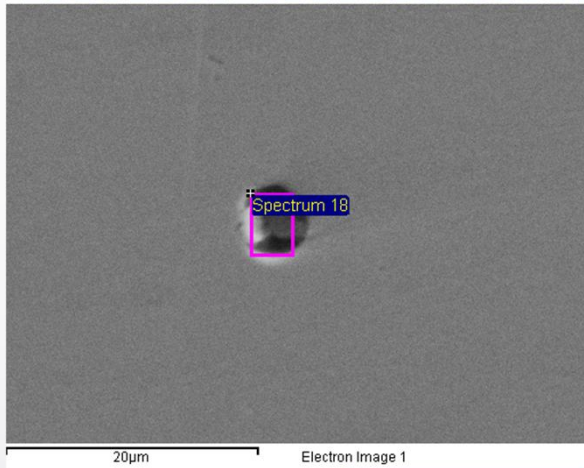
Inclusion classification: Oxide, sulfide, nitride

Steel composition in weight %: 0.097% C, 0.10% Si, 0.29% Mn, 0.015% P, 0.004% V, 0.027% Al, 0.008% S.

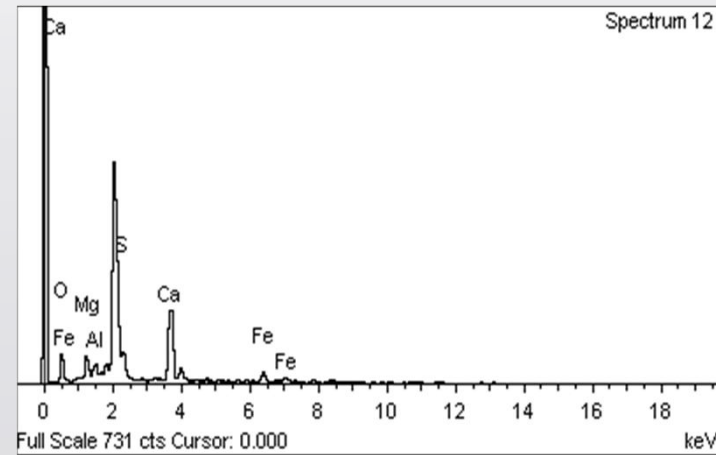
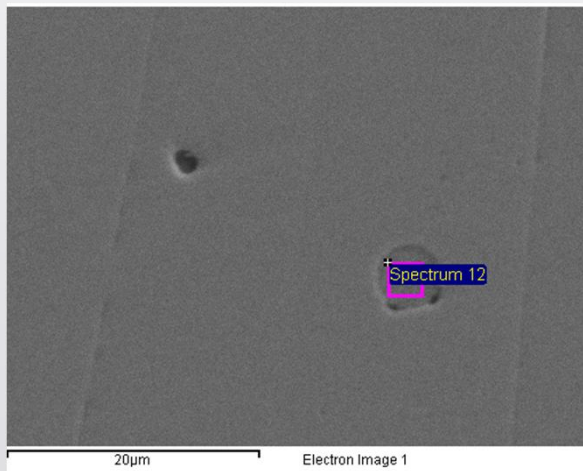
Complex non-metallic inclusions are considered to have at least a combination of oxide-sulfide or oxide-carbonitride or sulfide-carbonitride inclusions.

Therefore, the detected complex inclusions in the samples were classified into the following five groups: $\text{Al}_2\text{O}_3\text{-CaO-S}$, $\text{Al}_2\text{O}_3\text{-MgO-(Mn,Ca)S}$, $\text{Al}_2\text{O}_3\text{-MgO-MnS}$, MnS-(Ti,V)CN and $\text{Al}_2\text{O}_3\text{-(TiV)CN}$.

Inclusion Characterization in SEM and EDS

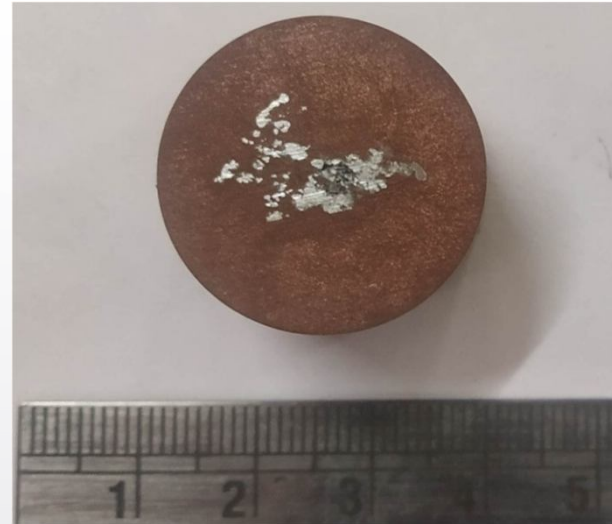


Element	O	Al	Ca	Fe
Weight%	22.29	30.17	1.01	46.53



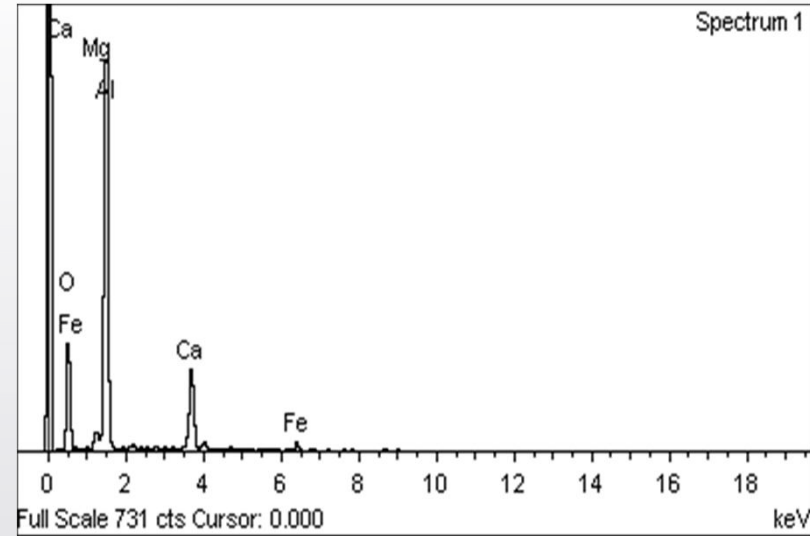
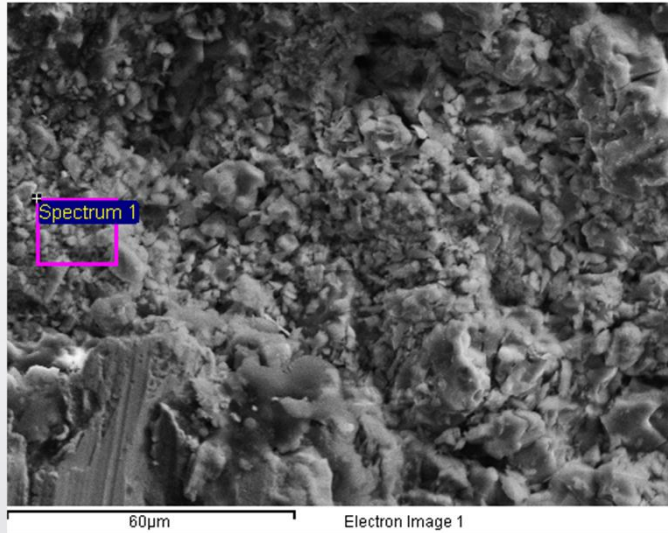
Element	O	Mg	Al	S	Ca	Fe
Weight%	44.41	7.25	3.16	7.13	28.04	10

SEN Clogging Material



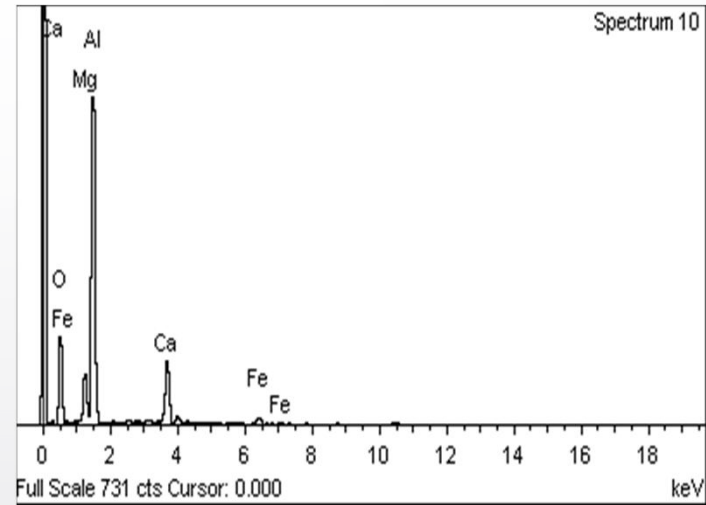
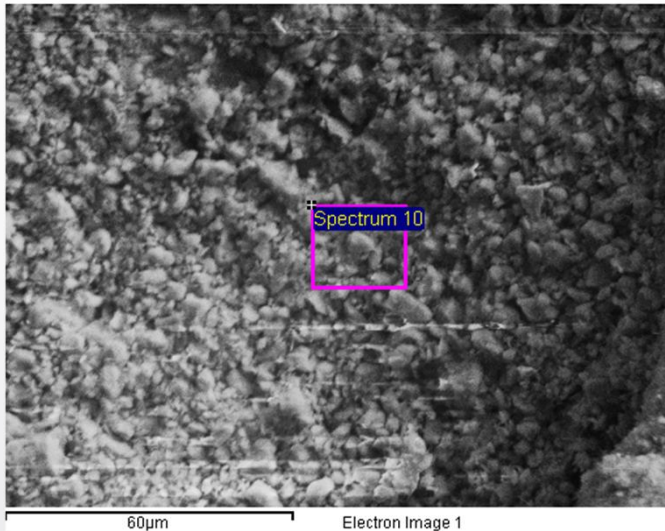
Sample	MgO%	Al ₂ O ₃ %	Fe ₂ O ₃ %
SEN Clog	5.06	47.23	37.94

SEN Clogging Material



Element	O	Mg	Al	Ca	Fe
Weight%	46.88	1.59	36.92	12.15	2.46

SEN Clogging Material



Element	O K	Mg K	Al K	Ca K	Fe K
Weight%	42.91	5.67	36.97	11.1	3.36

The clogged material analysis showed the material are close in chemical nature with the inclusions in steel. High amount of calcium Aluminates in both inclusion and clogged material was found along with some Alumina-MgO spinel. Spinel may be generated with the interaction with refractory and steel alumina inclusions.

Conclusion

- Presence of MgO in calcium aluminate inclusions often indicates exogenous sources since calcium containing deoxidizers are generally magnesium free. Calcium inclusions with high MgO content most likely originate from magnesia refractories by erosion or by reaction between slag and refractories.

Thank You



**International Conference on Future of Refractories in
Iron & Steel Industries
23-24 Sep 2022, Bokaro Steel City**